Faceting, Grain Growth, and Crack Healing in Alumina

Pankaj Rajak,*†‡, Rajiv K. Kalia,*†‡, Aiichiro Nakano,*†∥§, and Priya Vashishta†‡∥§

†Collaboratory for Advanced Computing and Simulations, ‡Department of Chemical Engineering & Materials Science, §Department of Computer Science, and DDepartment of Physics & Astronomy, University of Southern California, Los Angeles, California 90089-0242, United States

Supporting Information

ABSTRACT: Reactive molecular dynamics simulations are performed to study self-healing of cracks in Al2O3 containing core/shell SiC/SiO2 nanoparticles. These simulations are carried out in a precracked Al2O3 under mode I strain at 1426 °C. The nanoparticles are embedded ahead of the precrack in the Al2O3 matrix. When the crack begins to propagate at a strain of 2%, the nanoparticles closest to the advancing crack distort to create nano-channels through which silica flows toward the crack and stops its growth. At this strain, the Al2O3 matrix at the interface of SiC/SiO2 nanoparticles forms facets along the prismatic (A) ⟨1̅1̅10⟩ and prismatic (M) ⟨1̅0̅10⟩ planes. These facets act as nucleation sites for the growth of multiple secondary amorphous grains in the Al2O3 matrix. These grains grow with an increase in the applied strain. Voids and nanocracks form in the grain boundaries but are again healed by diffusion of silica from the nanoparticles.

KEYWORDS: ceramic nanocomposite, fracture, grain growth, reactive molecular dynamics, self-healing

There is a great deal of interest in designing material systems having the ability to sense and repair damage. Usually damage initiation involves the formation of defects such as dislocations, voids, and microcracks. These defects grow and coalesce to cause material failure. Taking a cue from biology, material scientists are developing novel self-healing systems to enhance reliability and lifetime of materials while reducing the cost of manufacturing, monitoring, and maintenance.1–4

Most of the approaches to designing self-healing material systems involve nanoscale or mesoscale containers filled with a healing material, which is released upon damage initiation either by an external stimulus (heat, light, and electric or magnetic field) or an internal change in the state of the system (pH, stress, or temperature).5–8 The healing material is transported to the damage site and immobilized after healing damage. Different materials require different self-healing conditions—ambient conditions for concrete, low temperatures for polymers, relatively high temperatures for metals, and very high temperatures for ceramics.

Here we investigate crack healing in a ceramic nanocomposite operating at high temperatures. Ceramics are lightweight, have high strength and stiffness, and can withstand high temperatures. However, technological applications of ceramics are limited by brittleness and sensitivity to flaws and cracks. Self-healing of defects and cracks can dramatically increase the reliability and lifetime of ceramics which, in turn, can reduce maintenance costs for a broad range of energy technologies from ceramic turbine blades to solid-oxide fuel cells.9,10

Crack healing has been examined in ceramic nanocomposites consisting of silicon carbide nanoparticles (n-SiC) or SiC whiskers in a silicon nitride (Si3N4) matrix,11,12 and also in an aluminosilicate glass containing vanadium–boride nanoparticles.13,14 Experiments have also been carried out to study crack healing in Al2O3 by n-SiC.15,16 Al2O3 has excellent mechanical properties (hardness, wear resistance) and oxidation resistance but low strength (σf = 400 MPa) and low fracture toughness (KIC = 3 MPa m1/2). Ando et al. measured the bending strength of sintered Al2O3/SiC composites from room temperature to 1300 °C.17–20 They introduced indentation cracks on Al2O3 surfaces and observed crack healing by n-SiC in the temperature range of 900 °C and 1300 °C. Precracked specimens were found to recover their static and fatigue strengths after crack healing. Three-point bending experiments on crack-healed samples showed the onset of fracture outside the crack-healed zone, whereas samples that had not gone through the crack-healing treatment

Received: April 3, 2018
Accepted: August 3, 2018
Published: August 3, 2018
prismatic (A) {1012} planes and that these facets have no orientational relationship with facets of alumina cavities which are parallel to {1012}, {1014}, and {0001} planes.

Crack healing begins with the diffusion of molten silica through the pinched-off region of alumina cavities (see Figure 1b). At the onset of crack healing, silica diffuses through nanopores that open up between the crack and the nearest alumina cavities. Unlike bulk, molten silica which consists of SiO$_4$ tetrahedra, silica in the cavities of alumina at 1426 °C consists of various SiO$_x$ fragments ($x = 0, 1, 2,$ and $3$). Figure 2a presents an atomic view of crack healing. Here black spheres represent the Al$_2$O$_3$ matrix and yellow, red and green spheres are Si, O, and C atoms, respectively. This snapshot, taken at a strain of 4%, shows crack blunting and the presence of SiO$_x$ fragments on crack surfaces. Figure 2b shows the effect of the applied strain on self-diffusion coefficients of SiO$_x$ in the direction of the crack propagation. The diffusion coefficient remains flat and the crack does not propagate for strains less than 2%. Above 2% strain the crack moves toward nanoparticles and self-diffusion coefficients of SiO$_x$ fragments in the...

fractured just below indentation cracks. Ando et al. have suggested a two-step process of crack healing: First, n-SiC are oxidized by atmospheric oxygen, and a 2–4 nm thick amorphous silica layer is formed around n-SiC; second, heat generated by oxidation and associated volume expansion produce molten silica which diffuses into cracks and heals them. Ando et al. find that the critical concentration of n-SiC for crack healing is between 15 and 20%. Experiments by Niihara et al. indicate that five percent volume fraction of submicrometer size SiC particles can increase the fracture toughness of alumina by 40% and strength by 1 GPa. In this paper we examine atomistic mechanisms of crack healing in Al$_2$O$_3$ by oxidized n-SiC and also grain nucleation and grain growth due to the presence of SiC in Al$_2$O$_3$. Prior to this work, we performed reactive molecular dynamics (RMD) simulation to study oxidation of n-SiC. Nanoparticles were cut out of cubic SiC crystal and placed in an oxygen rich environment. The chemical reaction

$$\text{SiC(s)} + \frac{3}{2}\text{O}_2(\text{g}) \rightarrow \text{SiO}_2(\text{s}) + \text{CO(g)}$$  

(1)

led to the formation of silica layers around n-SiC. The first few layers formed rapidly, but the growth slowed down due to limited diffusion of reactants to the n-SiC/SiO$_2$ interface. The thickness of the silica shell around n-SiC ranged between 2 and 4 nm, depending on the pressure and temperature of the oxygen environment. This is in good agreement with experiments of Ando et al.²⁰

RESULTS

Shapes of cavities in Al$_2$O$_3$ change dramatically under strain at 1426 °C. Figure 1a shows a snapshot of an atomic configuration of a cavity containing a n-SiC/SiO$_2$ nanoparticle (NP). The cavity is no longer spherical. It has facets parallel to prismatic (A) {1110} and prismatic (M) {1010} planes of crystalline $\alpha$-Al$_2$O$_3$. These results agree with transmission electron microscopy (TEM) studies of Hockey et al. on faceting of internal cavities in $\alpha$-Al$_2$O$_3$.²⁴ Analyzing the equilibrium Wulff shapes of cavities annealed at 1600 °C, they found well-developed facets in cavities smaller than 100 nm in diameter. Larger cavities did not exhibit faceting even on experimental time scales. Cavities are an order-of-magnitude smaller in our computer experiments, and therefore nucleation barriers are small enough for faceting transition to manifest on molecular dynamics (MD) time scales. This is consistent with theoretical calculations, which indicate that nucleation barriers for faceting decrease rapidly with a decrease in the cavity size.²⁵

Cavities near the crack facet differently from cavities farther away from the crack. This is due to the stress field of the crack. When the applied strain increases and the crack advances toward nearby cavities, the facets of cavities closest to the crack front first shrink in size and then merge to change the cavity shape from hexagonal to pentagonal; see Figure 1b. These faceting transitions are caused by surface diffusion of Al and O atoms. Our calculations show that surface diffusion coefficients of Al and O are $4 \times 10^{-7}$ and $2 \times 10^{-7}$ cm$^2$/s, respectively.

We also observe faceting of n-SiC at 1426 °C, but we do not find any correlation with the facets of alumina cavities in which nanoparticles are embedded. Kaplan et al. have experimentally observed faceting of submicron size SiC particles in internal cavities of $\alpha$-Al$_2$O$_3$.²⁶ Their high resolution TEM studies reveal that SiC particles develop facets parallel to {1011}, {1014}, and {1012} planes and that these facets have no orientational...
direction of approaching crack increase linearly with an increase in the applied strain; see Figure 2b. In addition, n-SiC diffuses into the crack front to stop crack growth. Some of the crack-healing features we observe are similar to those seen in fluorescent imaging of a crack in a silica film evaporated on PMMA containing polymer coated CdSe/ZnS NPs. The crack healing mechanism in the experiment involves diffusion of CdSe/ZnS NPs along the interface between silica and PMMA.

We have examined mechanical properties of Al2O3 after crack healing. Results for the stress—strain curve and nanoindentation response are presented in Figure S2 in the Supporting Information. The hardnes of the crack-healed Al2O3 composite is close to the hardness of pure α-Al2O3. This is consistent with the experiment of Ando et al.17–20

We have also examined changes in stress distribution between the crack front and NPs to gain insight into crack arrest and healing by Si and O diffusion. Figure S3b in the Supporting Information displays the stress component σzz between the crack tip and NPs as a function of the applied strain. The stress increases slightly when the strain is increased to 2%. At higher strains, however, σzz drops when nanopores nucleate in the alumina matrix between the crack tip and nearby cavities. At a strain of 4%, nanopores coalesce with the precrack and SiO2 fragments diffuse into the crack.

The presence of nanoparticles in faceted cavities gives rise to grain nucleation and grain growth in the strained alumina matrix. Snapshots in Figure 3a–d show nucleation of grains (blue) on facets normal to the direction of crack propagation. These grains are nucleated by the rotation of n-SiC inside the cavities.28,29 Inside the grains are under coordinated Al (5-fold) and O (3-fold) atoms due to broken Al–O bonds. Grains between neighboring n-SiC grow with an increase in the applied strains and coalesce at a strain of 4.4% (see Movie S1). Grain boundaries are amorphous, and they contain nanoscale pores at small strains which grow and coalesce to form secondary cracks at a strain of 4.8%. These cracks are also healed by silica diffusion from cavities.

We have examined stress distribution in the system to gain further insight into grain growth. The top panel in Figure 4a shows the stress component σyy in the x−z plane of the lower half of the system at an applied strain of 3.4%. (σyy is time-averaged virial stress in voxels of size 0.5 nm.) Stress is negligible around n-SiC (see the blue region in the bottom panel) and reaches 15 GPa approximately 10 nm ahead of the first row of n-SiC. The stress decreases away from the first row of nanoparticles and rises again reaching 12 GPa approximately 10 nm ahead of the second row of NPs.

The stress σyy correlates very well with damage evolution during grain nucleation and grain growth. Local damage31 is assessed by calculating the relative displacements of atoms under a uniform strain, εij:

\[
D^2(t, \Delta t) = \sum_{n=1}^{N} \sum_{i=1}^{3} \left[ r_i(t) - r_i(0) - \sum_{j=1}^{3} \sum_{k=1}^{3} \sigma_{ij} \delta_{jk} \right] \left[ r_i(t - \Delta t) - r_i(0) \right] \sum_{n} \left[ r_i(t) - r_i(0) \right] \left[ r_i(t - \Delta t) - r_i(0) \right]^{2}
\]

where

εij = \sum_{k} X_{ik} Y_{kj}^{-1} \delta_{jk} \tag{3}

and

X_{ij} = \sum_{n} \left[ r_i(t) - r_i(0) \right] \left[ r_j(t - \Delta t) - r_j(0) \right] \tag{4}

Y_{ij} = \sum_{n} \left[ r_i(t) - r_i(0) \right] \left[ r_j(t - \Delta t) - r_j(0) \right] \tag{5}

Here \( r_i \) and \( r_j \) are atomic coordinates in the unstrained and strained systems, respectively, and the summation over \( n \) includes all atoms within the range of interaction. Equation 2 is minimized with respect to \( \epsilon_{ij} \) to obtain \( D_{min}^{2} \).

The bottom panel of Figure 4b shows the minimized values of eq 2 along the basal (0001) and prism (2110) planes of a section of Al2O3. Here green and blue regions correspond to \( D_{min}^{2} = 1.5 \) and \( D_{min}^{2} = 0.25 \), respectively. The maximum deformation occurs along the slip direction [011] of the prism plane of α-Al2O3 (see Supporting Information Figure S4(a), Movie S2).32–34 These deformation values correlate very well with changes in \( \sigma_{yy} \) in the x−z plane.

We have also investigated the effect of three and four rows of NPs on damage mitigation in the alumina matrix. The diameter of each NP (7 nm) and the distance between NPs (2 nm) are kept the same. Recall, with a single row of NPs, silica heals the precrack but damage appears approximately 65 nm ahead of the NPs above a strain of 3.5% and alumina matrix fractures at a strain of 4.5%. A crack develops and propagates on the prism plane along the slip direction [011] due to the formation and coalescence of nanovoids along the [011] direction. In the case of two rows of NPs, cracks appear
and propagate directly ahead of the second row of nanoparticles; see Figure 5a and Movie S3. The damage zone starts around 100 nm ahead of the precrack. Another row of NPs shifts the damage zone further to 130 nm. Finally, with four rows of nanoparticles the system is healed and there are no cracks in the alumina matrix at 5% strain; see Figure 5b and Movie S4. The damage is only in the form of nanovoids in between the rows of n-SiC, but silica diffusion heals them and prevents crack growth. When the strain exceeds 5%, secondary cracks appear in grain boundaries, but they are also healed by silica diffusion from nearby cavities.

CONCLUSION

In summary, RMD simulations of Al2O3 containing SiC/SiO2 nanoparticles show that silica is an excellent healing agent of cracks in alumina at high temperature. When the applied strain is increased, bonds break and nanovoids are formed in the alumina matrix between the crack front and nanoparticles. These nanovoids are the conduits through which silica diffuses into the crack to stop its growth. The self-diffusion coefficient of silica is liquid-like (>10\(^{-5}\) cm\(^2\)/s), and it increases rapidly with an increase in the applied strain. As a result, the higher the applied strain, the more rapid the crack healing. RMD simulations also show that alumina cavities containing SiC/SiO₂ nanoparticle are faceted, and the low energy prismatic (A) \{2110\} and prismatic (M) \{1010\} planes are the prominent facets. These results are consistent with TEM studies of nanocavities in \(\alpha\)-Al₂O₃. We observe grain formation on facets and grain growth with an increase in the strain. Damage in the form of nanovoids and nanocracks is observed in grain boundaries, but rapid diffusion of silica from
ASSOCIATED CONTENT

Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acsnano.8b02484.

Simulation details, description of interaction potential for Al₂O₃, SiC, and SiO₂, and structural analysis of alumina inside the amorphous grain (PDF)

Movie showing nucleation and grain grown of amorphous grains (AVI)

Movie showing stress distribution and local damage in Al₂O₃ (AVI)

Movie showing crack propagation in Al₂O₃ containing 2 rows of nanoparticles (AVI)

Movie showing crack propagation in Al₂O₃ containing 4 rows of nanoparticles (AVI)

AUTHOR INFORMATION

Corresponding Authors
*(P.R.) E-mail: rajak@usc.edu.
*(R.K.K.) E-mail: rkalia@usc.edu.

ORCID
Pankaj Rajak: 0000-0002-6344-6056
Aiichiro Nakano: 0000-0003-3228-3896
Priya Vashishta: 0000-0003-4683-429X

Author Contributions
P.R. carried out the MD simulations and analyzed the results.
P.R., R.K.K., A.N., and P.V. designed the MD simulation study.
P.R., R.K.K., A.N., and P.V. advised this work. All authors contributed to analyzing the results and writing the manuscript.

Notes
The authors declare no competing financial interest.

ACKNOWLEDGMENTS

The work was supported by the grant DE-SC0018195 funded by the U.S. Department of Energy, Office of Science. Simulations were performed at the Argonne Leadership Computing Facility under the DOE INCITE program and at the Center for High Performance Computing of the University of Southern California.

REFERENCES


